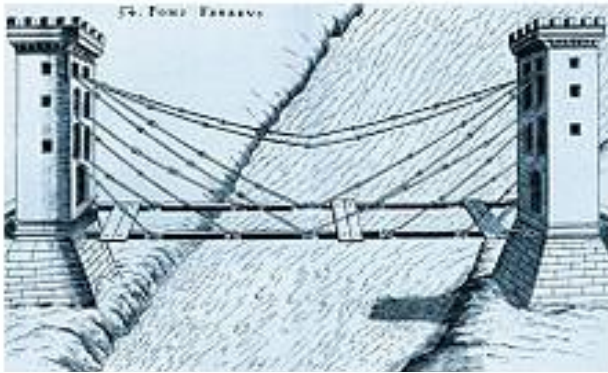


Where are the Stay Cables? An Investigation.



Khaled Shawwaf
Technical Director & Vice President (Retired)

2015 PTI Convention- Houston, April 26- 28



The first known drawing of a cable stayed bridge: by Fautus Verantius, ~1595, Venice
Span estimated about 30 meters



The first modern cable stayed bridge !
Stromsund Bridge, 1956 - 182 m



The longest cable stayed bridge !
Russky Bridge, 2013 - 1104 m



Cable Stayed Bridges are very efficient
and visually attractive !

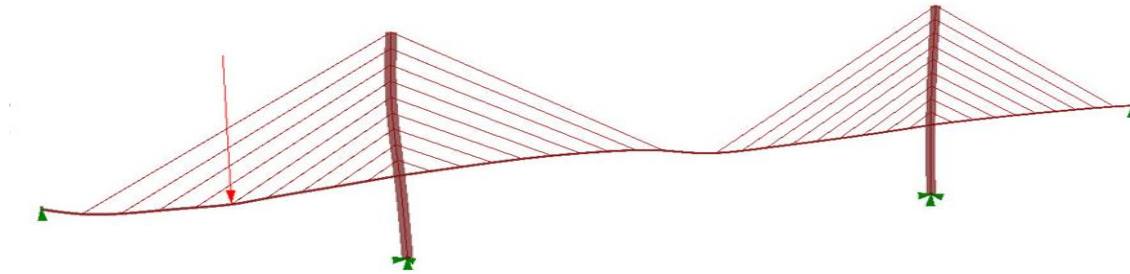
As spans get longer there are increased
demands on the performance
of the stay cables

Longer spans are more flexible

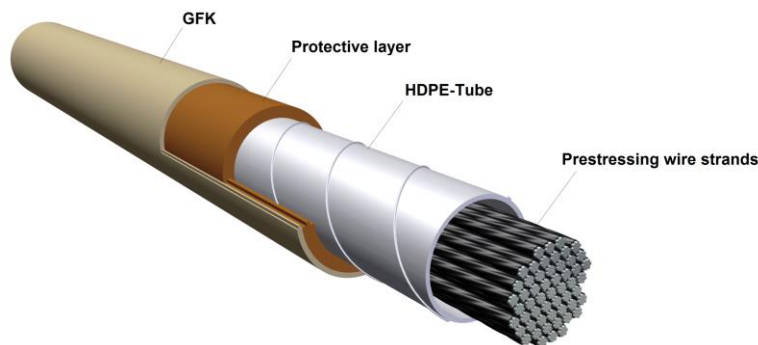
Large displacements & rotations

Longer cable lengths result in large
changes in sag

Cable systems should have
enhanced performance to meet
these demands



- In the global analysis of the bridge, cables are usually modeled as line members with axial stiffness only -> Hinge ends !
- This is acceptable and leads to accurate results for the sectional forces of the bridge members and the axial forces in the cables
- In reality, cables have a significant flexural stiffness and are subjected to static and fatigue bending stresses that may be significant -> Fixed ends !

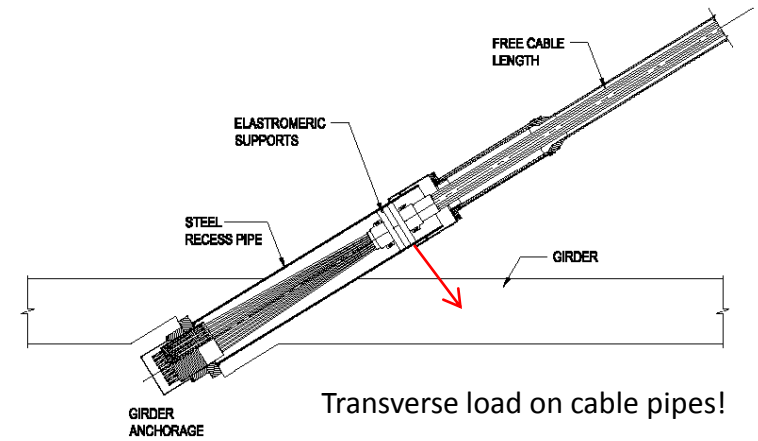


What causes these bending stresses?

PERMANENT BENDING STRESSES, f_c :

Fabrication and construction tolerances

- *Discussed in this paper!*

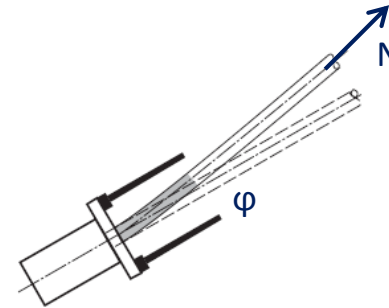


VARIABLE BENDING STRESSES, f_v :

Angle Change at the anchors due to:

- Change in axial force and sag
- Structural displacements and rotations
- Differential temperature
- Cable oscillations

- *Not discussed in this paper!*

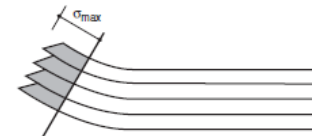


Fixed Support !
Bending stresses:
local and depend
on N , φ and E

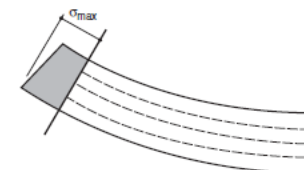
DEVICES TO REDUCE BENDING STRESSES f_v :

Elastic supports for strands at anchorages

- *Discussed in this paper!*



$$2 \cdot \varphi \cdot \sqrt{E \cdot \sigma_a}$$



Bending stresses
are independent
of cable stiffness!

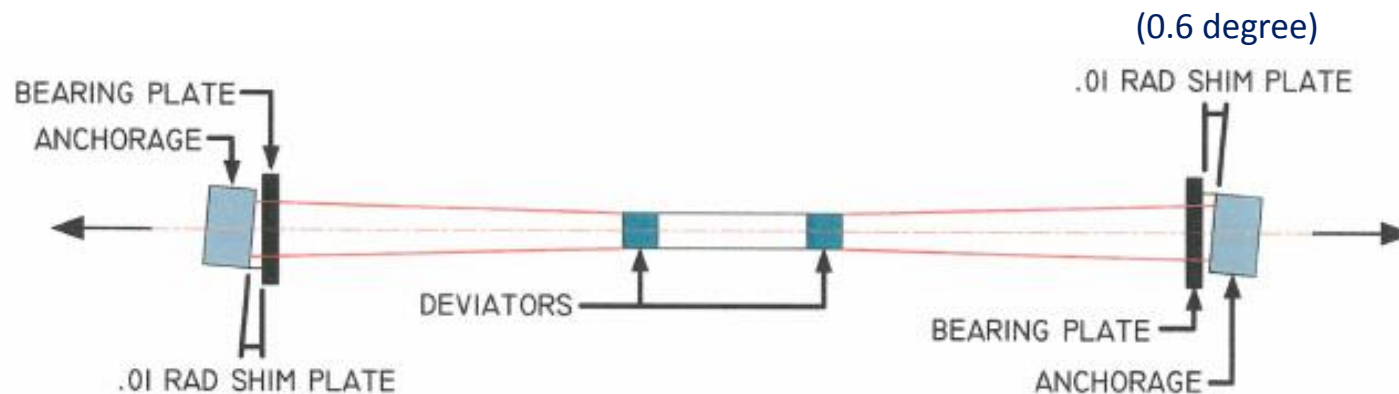
PTI DC45.1-12

Recommendations for Stay Cable Design, Testing and Installation

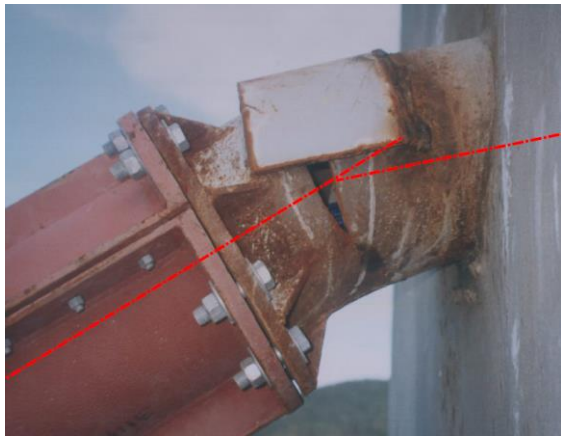
Section 4.2: Acceptance Testing of stay cables

Tests of 3 representative stay cable specimens shall be carried out...

...The anchorages of the stay cable specimens shall be supported on wedge-shaped shim plates, creating angular deviations of 0.01 radians...

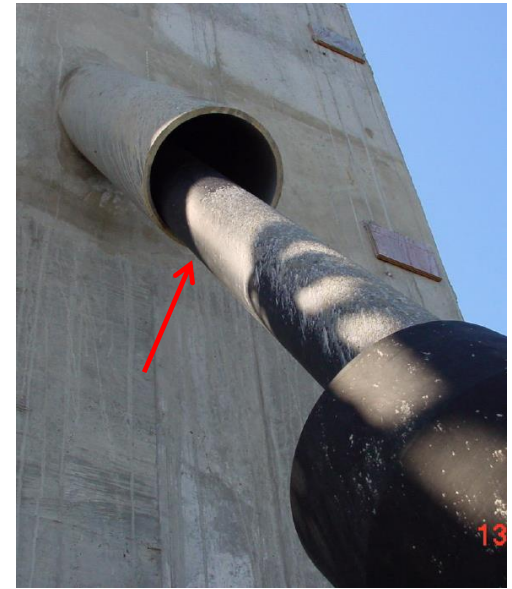


Test: 2 million cycles of fatigue loading and subsequent tensile strength

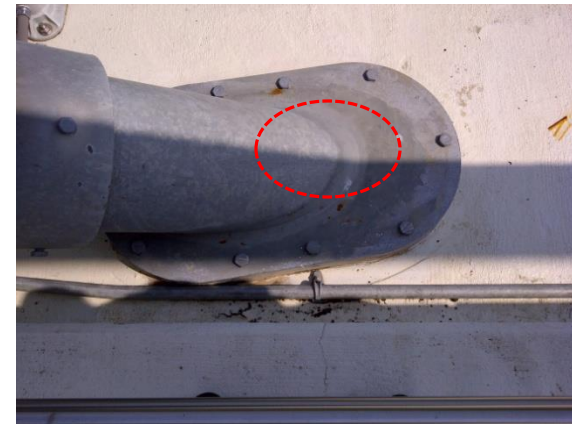


Mexico: To correct deviation the recess pipe was cut and bent about 20 degrees. Discovered by DSI during inspection some years after bridge completion.

USA: East Coast.
No room to place the neoprene bearing discs. Heat bending was considered to realign the pipe.



USA: Bridge in Midwest.
Cable deviation was too large. Pipe cut at top of deck, welded to oval plate and bolted down.



Things don't always work out !

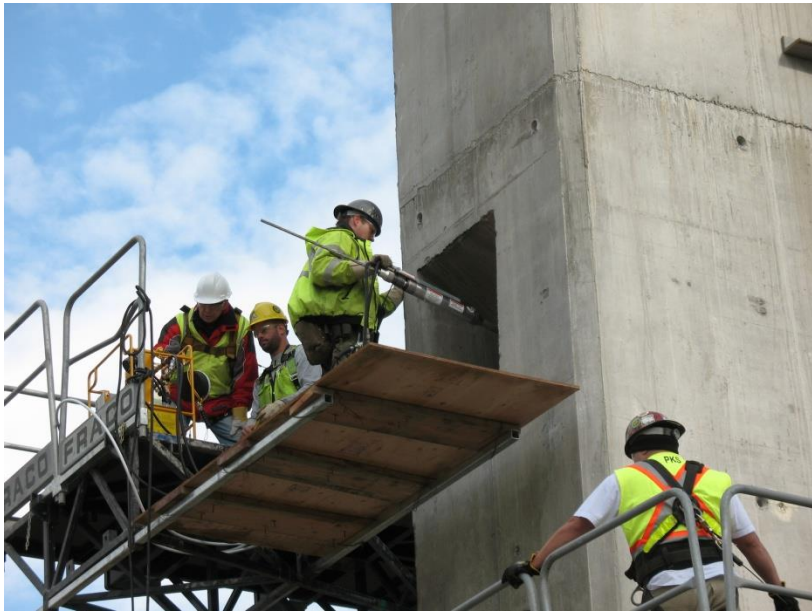
How large are actual cable deviations ?

No data is available !

During construction of Pitt River Bridge, DSI measured the position of all 96 cables at the tower and deck level after final stressing



- Pitt River Bridge, Vancouver, BC: 96m + 190m + 96 m. Composite steel deck & concrete towers.
- Cables: Middle plane ~60 strands and sides are ~30 strands; 8 cables each side of towers. Total= 96.
- Cables cross each other in the towers and anchored in a welded steel assembly at the deck.



Cable Installation



Finished Cables





Strands compacted
into hex pattern

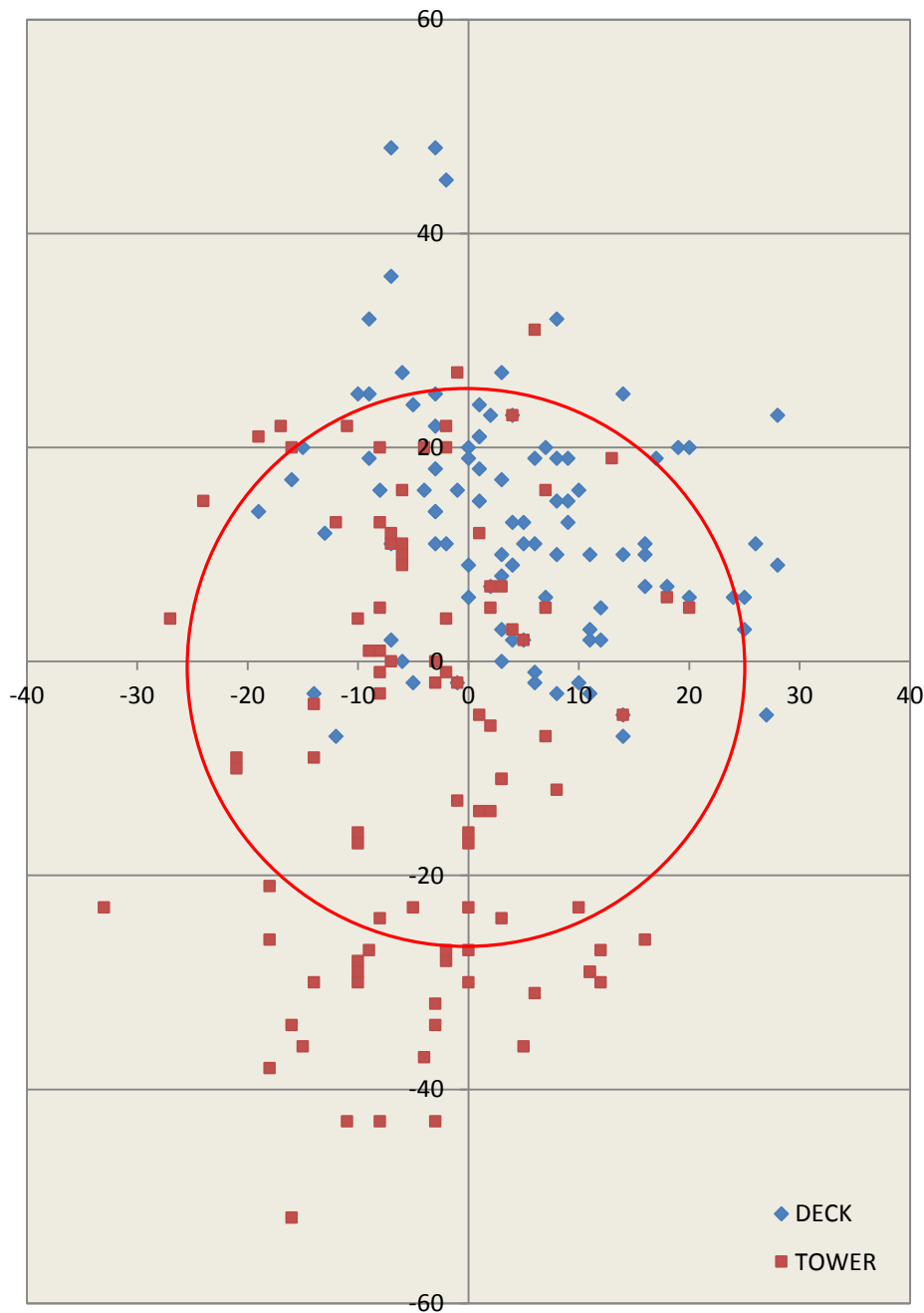
Tower showing
steel Exit pipes
& stressing tails



Measuring device
bolted to anchorage
at deck level

Bolted clamp- with exit
and recess pipes

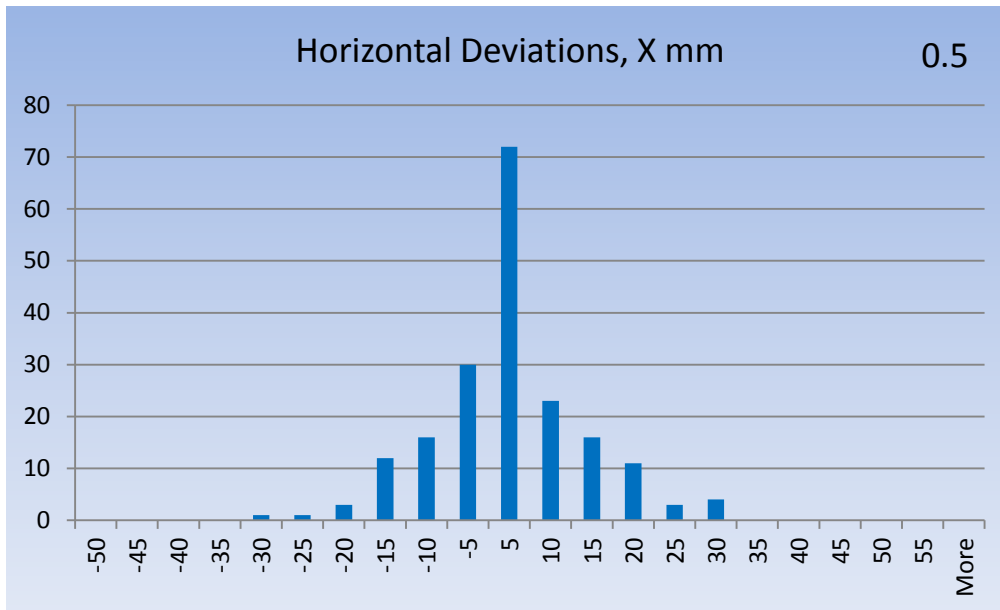




Measurement Data, mm

- 96 measurements each at towers and deck = 192 Total
- Location of measuring points from face of anchors: Towers: 3.13 to 5.35 m
Deck : 1.42 & 1.98 m
- Limit shown in red: 25 mm
- Differences between Deck and Tower !
- Accuracy ± 5 mm !

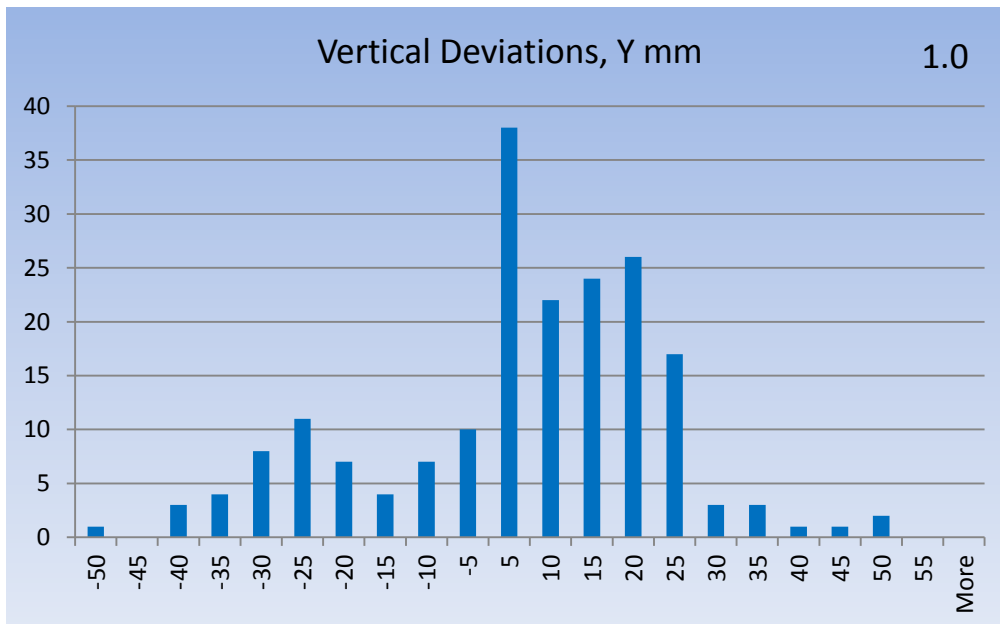




Horizontal Deviations, X mm:

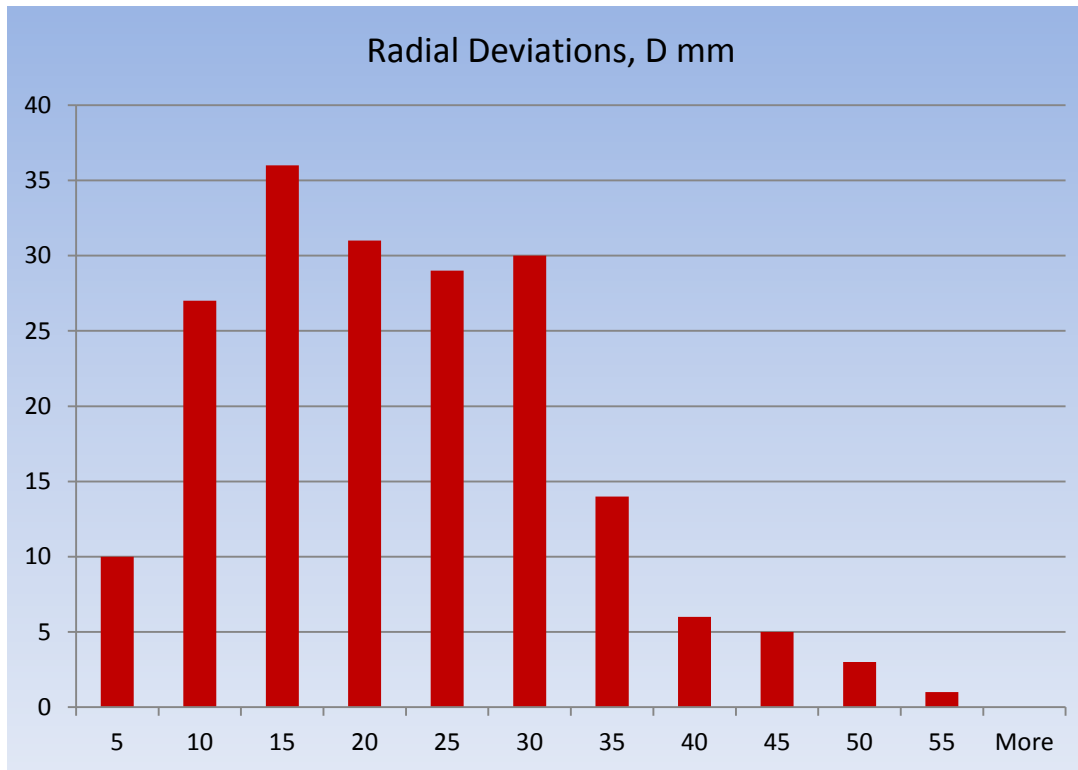
- Almost perfect bell curve
- Variation between -30 to +30 mm
- About **74%** are less than < 10 mm
- Only influenced by setup accuracy

Total number of Data: 192

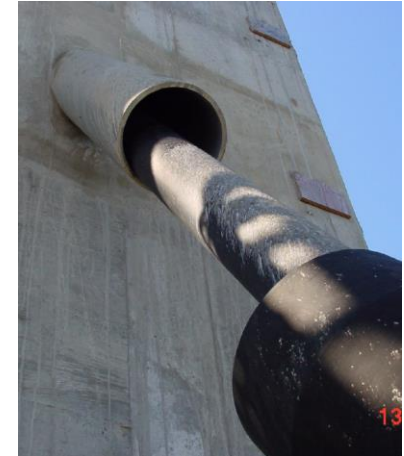


Vertical Deviations, Y mm:

- Unsymmetrical distribution
- Variation between -50 to +50 mm
- About **37%** are less than < 10 mm
- About 62% are +ve: High
- Influenced by many factors !

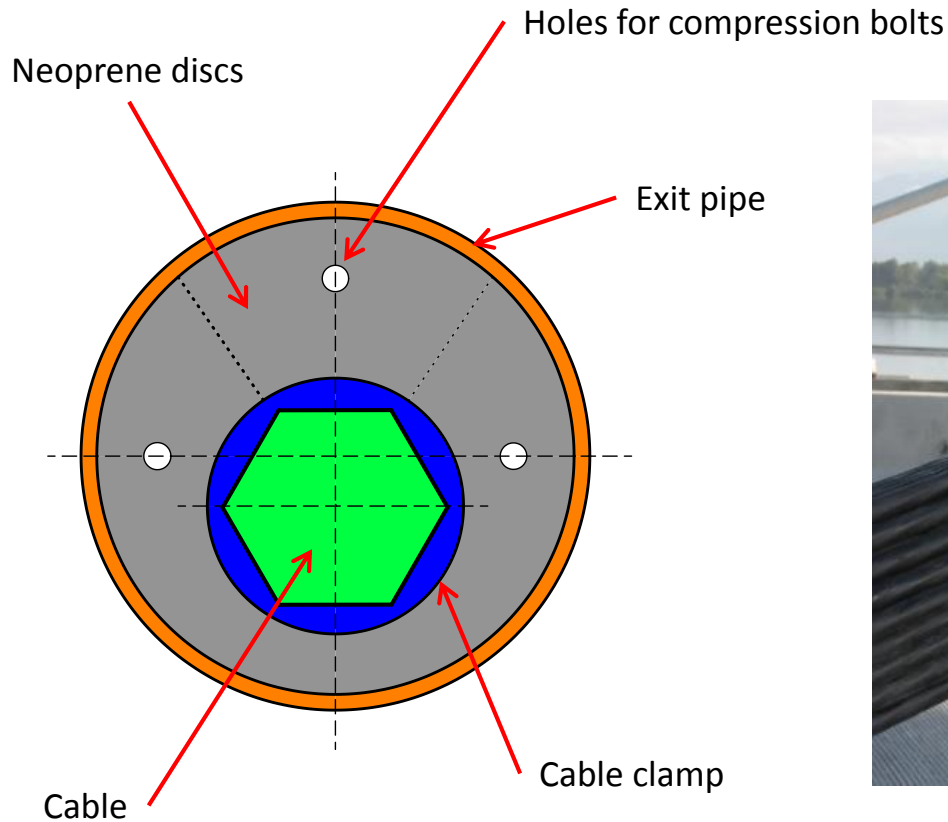


Total Number = 192:
96 readings each at the
towers and deck level



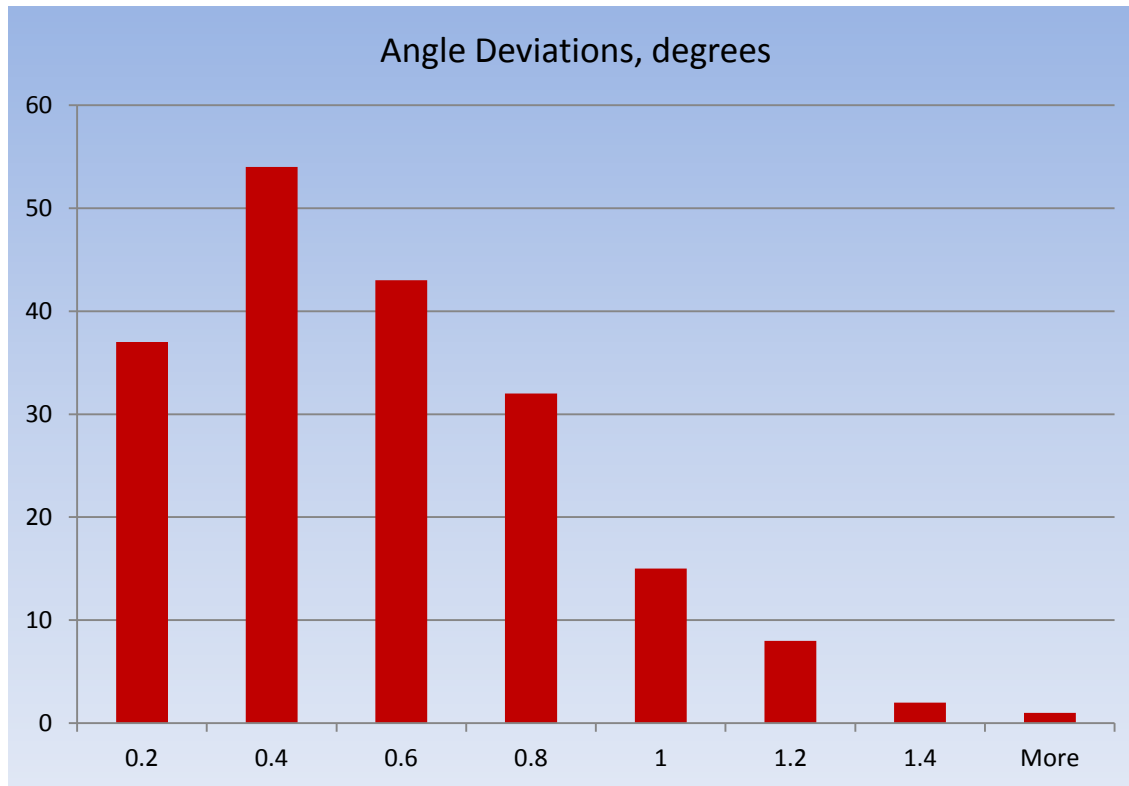
Radial Deviations, D mm:

- About **33%** > 25 mm and **7.8%** > 35 mm. Maximum deviation **55 mm**
- Excessive deviations makes it difficult to install neoprene bearings and dampers
- Adjustability should be provided to accommodate these deviations !
- How was this provided in Pitt River Bridge cables?



Cable adjustability for the Pitt River Bridge:

- Compressed neoprene discs act as visco-elastic damper – Short & medium length cables
- Based on field measurements, eccentric holes were cut in the neoprene discs
- This allowed large adjustability without changes to the recess/exit pipe connection flange
- Holes in neoprene discs are cut by water jet: accurate and fast. Accommodated 55 mm!



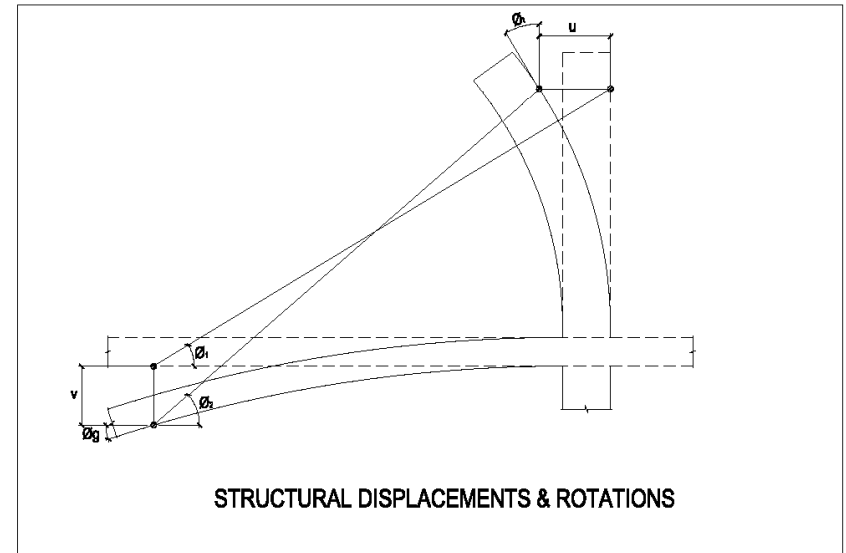
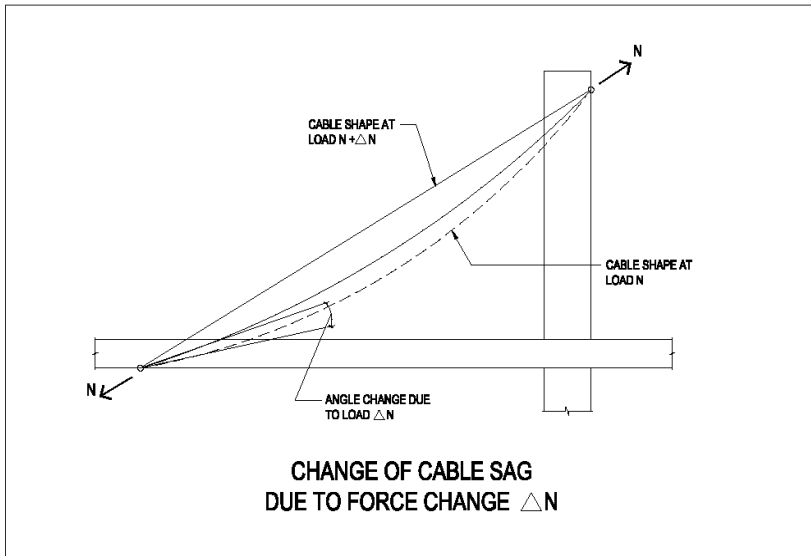
Total Number = 192:
96 readings each at the
towers and deck level

Bending stress:

$$2 \cdot \varphi \cdot \sqrt{E \cdot \sigma_a}$$

Angle Deviations, φ degrees:

- About **28%** > 0.6 degrees, and **8.9%** > 0.8 degrees
- Some deviations exceed the values used in the PTI cable acceptance tests !
- *Impact of temperature and actual cable force on cable position and measurements !*
- Built in angle deviations φ cause permanent static bending stresses in the strands
- Permanent bending stresses cause fretting that may reduce strand fatigue life
- Let us take a look at bending stresses that occur during service stage



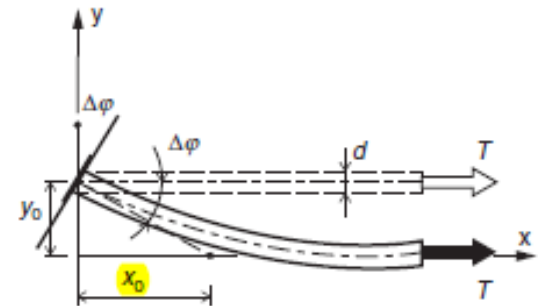
Cable bending stresses during service are due to angle changes in the cables

Consider an angle change $\varphi = \underline{1.0 \text{ degree}} = 0.0175 \text{ radians}$

Axial stress in the cable $\sigma_a = \underline{0.4 \text{ fsu}} = 744 \text{ Mpa}$

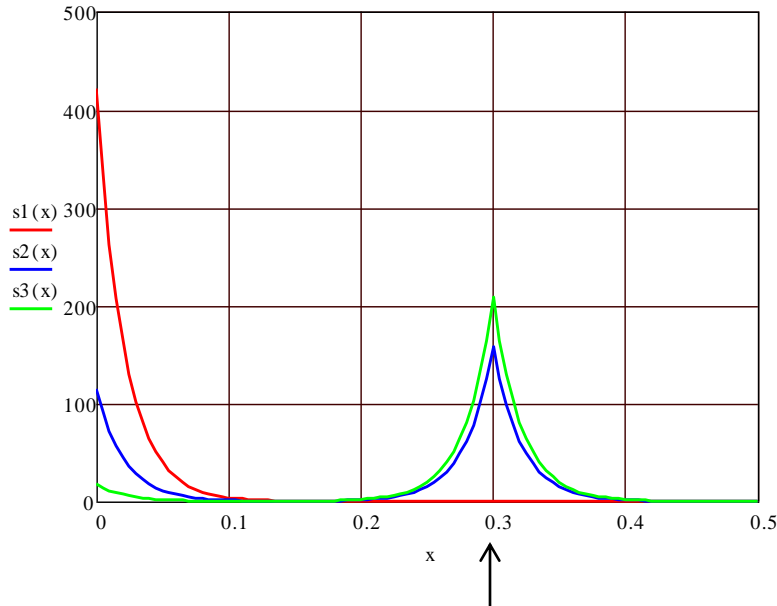
Elastic modulus of the strands $E = 195,000 \text{ MPa}$

$$\begin{aligned} \text{Bending stress at the anchorage} &= 2 \cdot \varphi \cdot \sqrt{E \cdot \sigma_a} \\ &= \mathbf{422 \text{ Mpa}} = \underline{0.23 \text{ fsu}} ! \end{aligned}$$



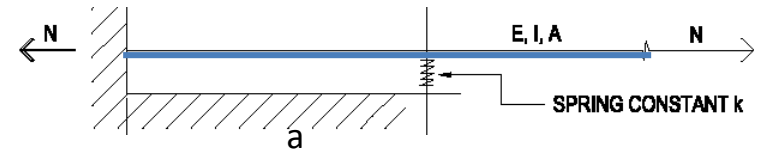
- Some measures are provided to reduce this bending stress. **How?**
- Provide flexible support to the strands some distance in front of the wedges !

Bending Stress MPa, 1.0 deg, N=0.4 Pu

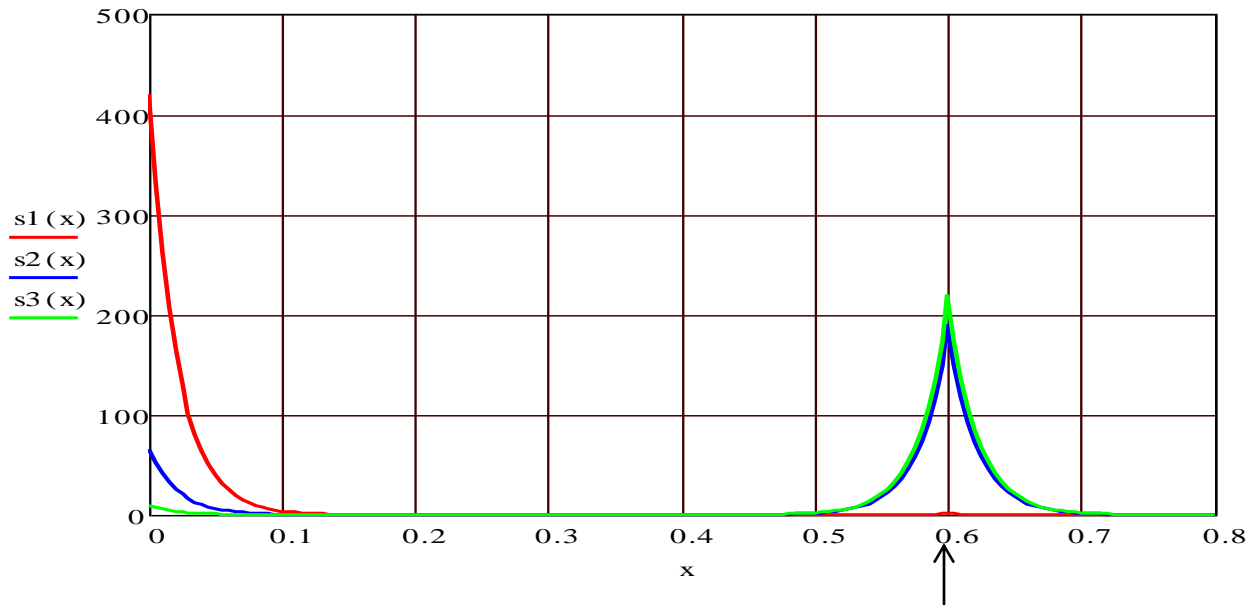


Cable Bending Stresses- Vary k & a :

- Angle change 1.0 degree
- Axial load $N = 0.4 P_u$ (PTI allowable 0.45)
- Effects of support location a : 300 & 600 mm
- Effects of support stiffness k : 1000 & 5000 kN/m
- Stress at anchor reduces to less than 20%
- Stress at support about half of $k = 0$!
- Design stress at support is less than peak shown

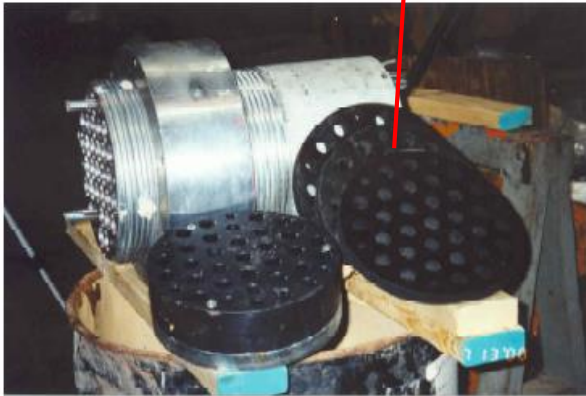
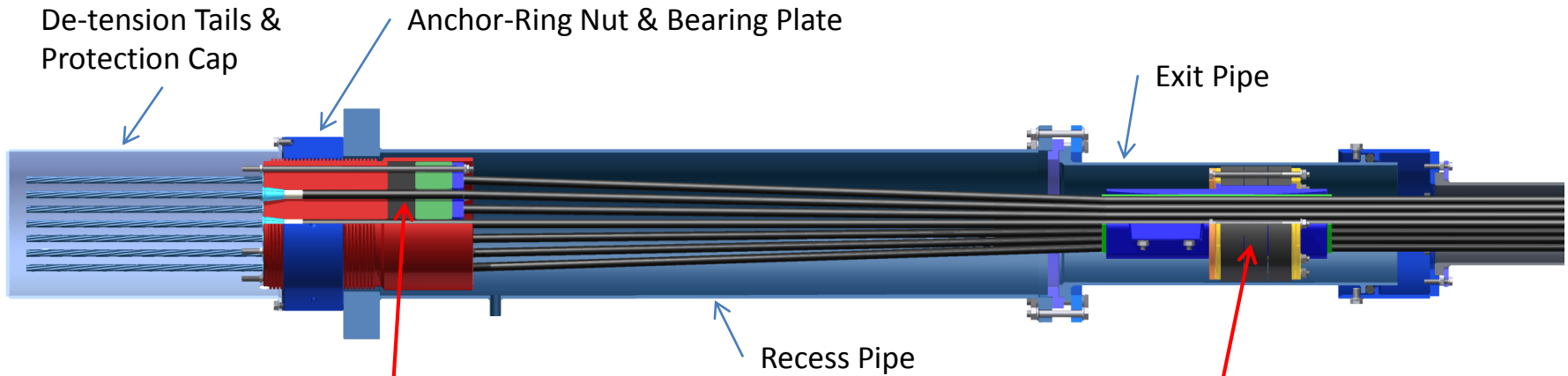


Bending Stress MPa, 1.0 deg, N=0.4 Pu



Support Stiffness:

- No Support, $k = 0$
- $k = 1,000$ kN/m
- $k = 5,000$ kN/m



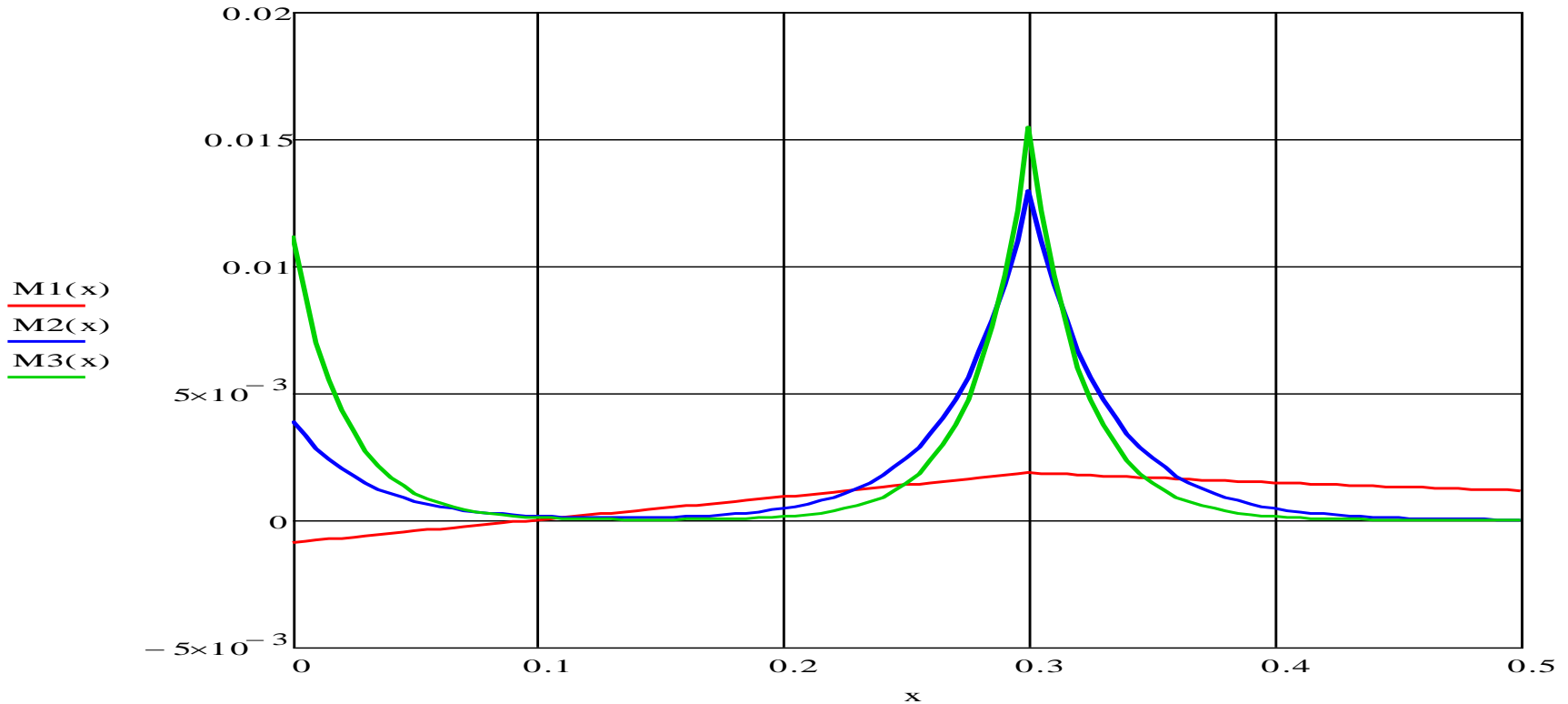
Neoprene discs inside anchors are compressed after strand installation. Provide flexible lateral support to the strands and seal the anchor body.

DSI
Cable System



Visco-elastic (rubber) damper installation becomes difficult with large deviations

Bending Moments, kN.m



- No Axial Force
- $N = 0.2 P_u$, kN
- $N = 0.4 P_u$, kN

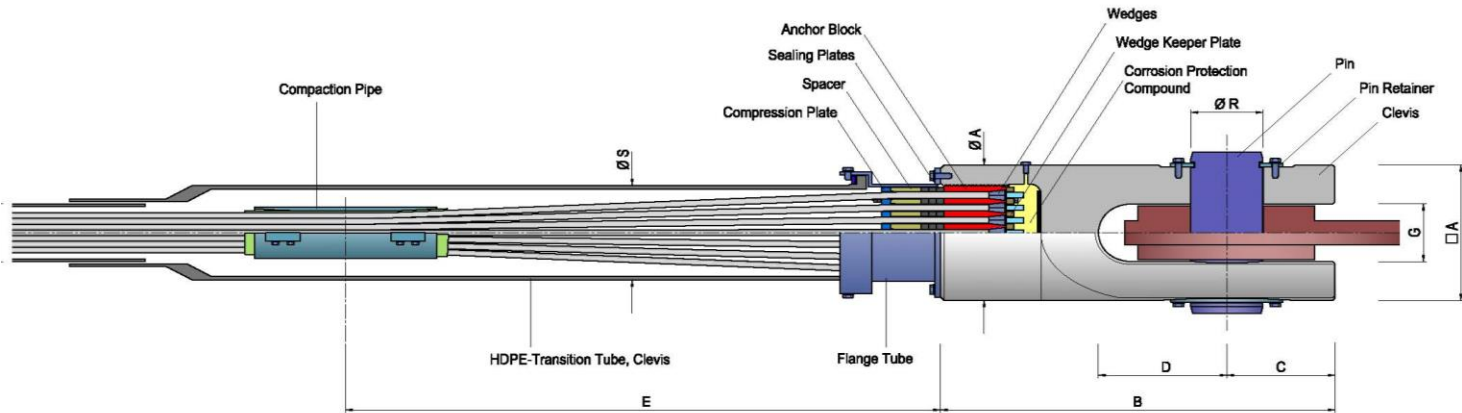
Effects of cable axial force on Bending Moments:

- Angle change = 1.0 deg & Support stiffness = 1,000 kN/m
- Flexible support location at 300 mm from wedges
- When $N = 0$, cable behaves like a beam: simple bending
- Axial force tends to magnify and localize bending

Cable Bending: complex interaction between N , k and support location 'a'



Clevis Cable System 7 to 91 Strands



There is a way to avoid Bending Moments
in Cables by using Clevis anchorages



Provencher Bridge



SUMMARY: Cable Bending

- Imposed rotations at ends cause bending stresses in cables
- Axial force magnifies & localize bending stresses in stay cables
- Fabrication and construction tolerances result in permanent bending stresses
- Field measurements of cable deviations were made on 192 anchorages
- During service, angle changes at ends cause transient bending stresses:
 - * Structural displacements & rotations due to Live Loads
 - * Sag variations due to LL and differential temperature
 - * Cable oscillations- wind induced and parametric
- Bending stresses impact the Strength and Fatigue design of cables
- Cable anchorages should include means to reduce bending stresses



Thank You